Reactive Transport Modeling:

Arsenic in the Red River Floodplain, Vietnam

Jordan Dahle

NDSU Geochemistry GEOL 628 2020

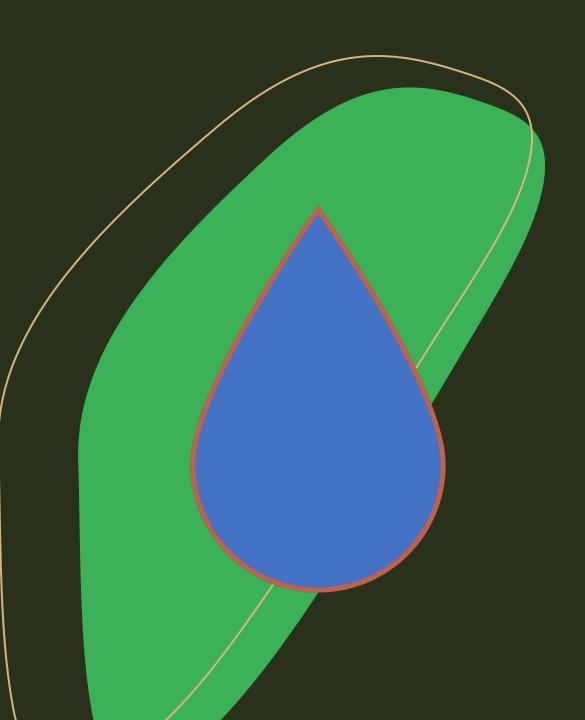


Red River Floodplain

- Major Population Centers
 - Hanoi, Vietnam

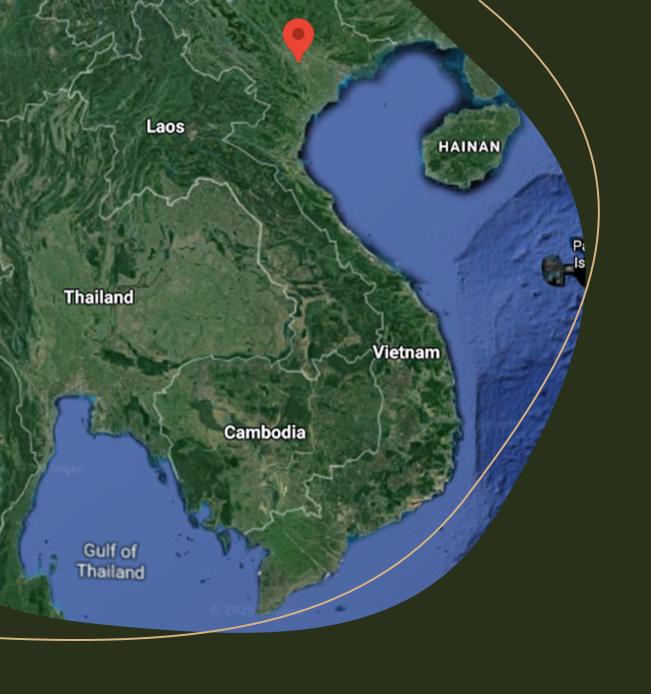
 Up to 11 million people at risk of arsenic exposure (Postma et al. 2007)

WHO drinking water limit 10 μg/L



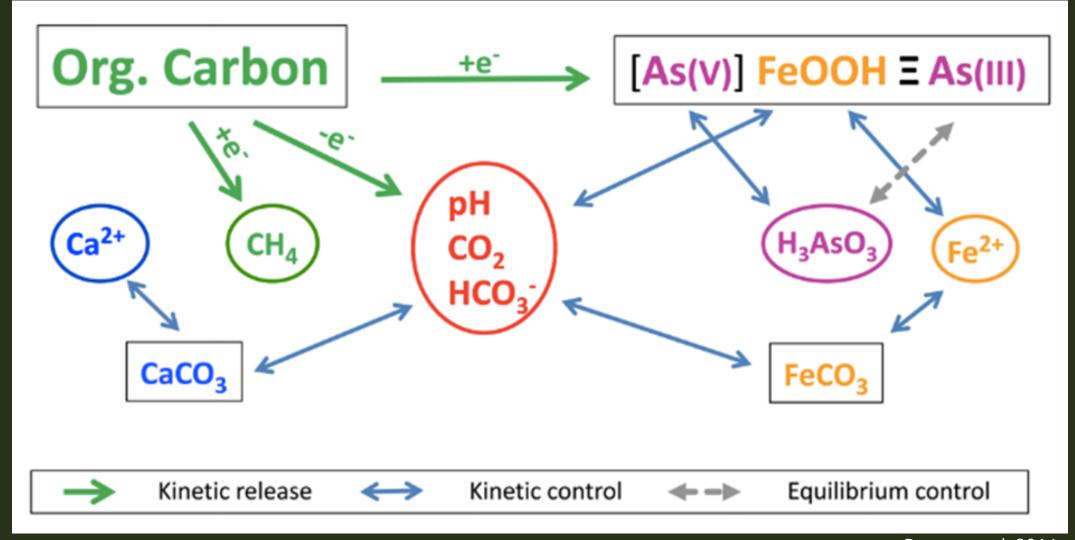
Red River Floodplain Aquifers

- Holocene Aquifers
 - Deposited 500 6000 yrs ago
- Sandy fluvial channel and sand bar deposits overlain by clay overbank deposits
- Recharged through outcropped sand or fractured clay
- Anoxic aquifer conditions



Past research

- Complicated hydrological conditions
 - Channel modification
 - Agriculture
- Three arsenic mobilization theories
 - Fe-oxide reduction
 - Sediment desorption within aquifer
 - Mobilization at surface

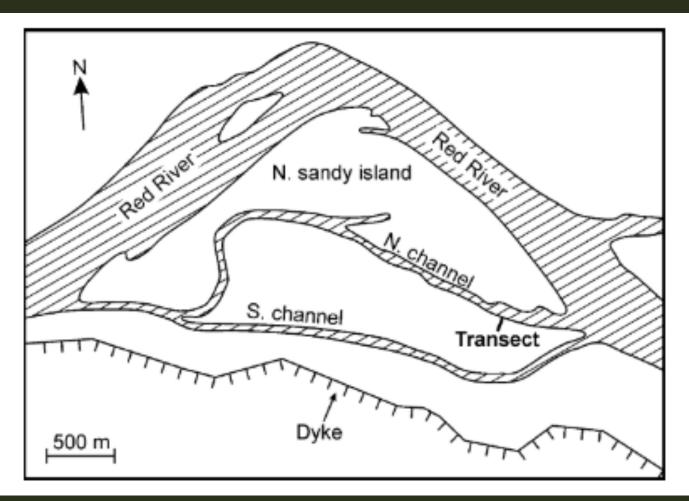


Postma et al. 2016

Schematic of Key Processes

Arsenic in groundwater of the Red River floodplain, Vietnam: Controlling geochemical processes and reactive transport modeling

Postma et al. 2007



Goals:

- Analysis of groundwater chemistry
- PHREEQC transport modeling
 - Arsenic mobilization and transportation
 - Fit model to field observation

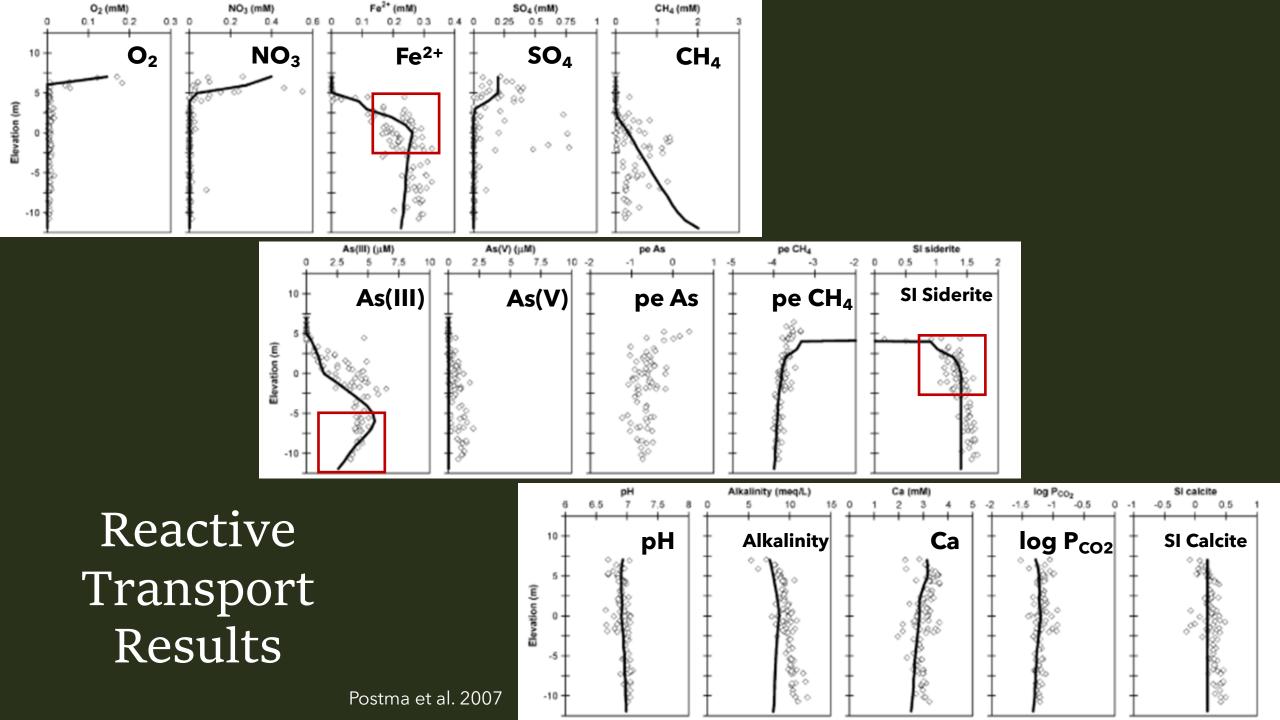
Postma et al. 2007

Table 2 Water composition in the Red River and in the groundwater of borehole H51 at elevation 0.3 m (Fig. 2)

	River water	Ground water
EC (μS/cm)	290	880
Temp. (°C)	30	26.4
O ₂ (mmol/L)	0.3	0
pH	7.18	6.95
As total (µmol/L)	< 0.01	5.4
As(III) (µmol/L)	_	4.6
Fe(2+) (mmol/L)	< 0.001	0.27
Mn (mmol/L)	< 0.0009	0.001
Ca (mmol/L)	0.53	2.76
Mg (mmol/L)	0.18	1.91
Na (mmol/L)	0.2	0.23
K (mmol/L)	0.04	0.1
NH ₄ (mmol/L)	< 0.006	0.17
Alkalinity (meq/L)	2.38	10.2
SO ₄ (mmol/L)	0.06	0
Cl (mmol/L)	0.11	0.08
NO ₃ (mmol/L)	0.01	0
PO ₄ (mmol/L)	< 0.001	0.010
Si (mmol/L)	0.27	0.57
CH ₄ (mmol/L)	_	0.57
SI calcite	-0.64	0.26
$\log P_{\rm CO_2}$	-1.98	-1.18

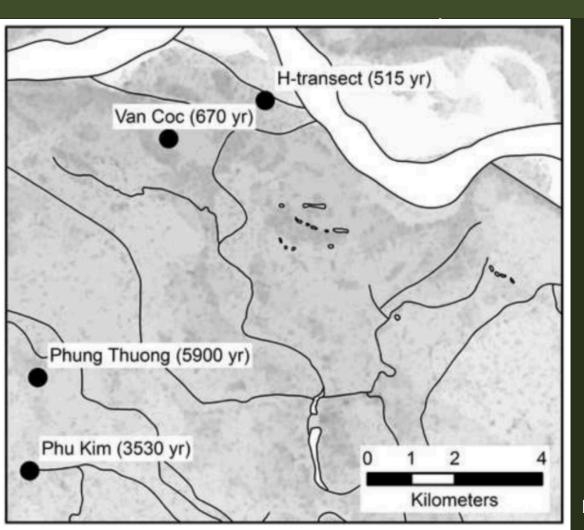
Geochemical Analysis

Postma et al. 2007



A model for the evolution in water chemistry of an arsenic contaminated aquifer over the last 6000 years, Red River floodplain, Vietnam

Postma et al. 2016



Goals:

- Model full range of depositional ages
- Improve model with kinetic reactions

Postma et al. 2016

- Surface Master Species
 - Langmuir ArsenicSpeciation
- Surface Species
 - Speciation Reactions
- Phases
 - Define Kinetic Reactions

```
#database LangmuirAs_wateq4f.dat
SURFACE_MASTER_SPECIES
Langmuir Langmuir
SURFACE_SPECIES
Langmuir = Langmuir
Langmuir + H3AsO3 = LangmuirH3AsO3
-log_k 3.176
-mole_balance LangmuirH3AsO3
```

- Solution Composition
 - Infiltrating
 - Initial Groundwater
- Surface
 - Surface Site Density
- Equilibrium Phases
 - Equilibrate with CO₂

```
solution 0
             #Red River water (Postma et al. 2007, GCA v71.5054-)
temp
units mmol/1
рΗ
      7.18
0(0) 0.4
      0.53
Mg
Na 0.2
K 0.04
Alkalinity 2.38
#S(6) 0.06
C1 0.11
#N(5) 0.01
Si 0.27
SOLUTION 1-40
      mmol/1
      7.18
As le-10
      0.53
    0.18
Na 0.2
K 0.04
Alkalinity 2.38
C1 0.11
Si 0.27
```

```
SURFACE 2-40
Langmuir Fe(OH)3As kin 0.07 8.9e3
-no_edl
-equilibrate 1
```

```
EQUILIBRIUM_PHASES 1
CO2(g) -1.1 30
```

Rates of Kinetic Reactions

•
$$-\frac{dC_{CaCO_3}}{dt} = m_o * 2.38 * 10^{-11} * \frac{m_t^{3.0}}{m_o} * (1 - SR_{CaCO_3})$$

•
$$-\frac{dC_{FeCO_3}}{dt} = 3.17 * 10^{-12} * (1 - SR_{FeCO_3})$$

•
$$-\frac{dC_{FeOOH}}{dt} = m_o * 2.54 * 10^{-11} * \frac{m_t^{1.5}}{m_o} * (1 - SR_{FeOOH})$$

•
$$-\frac{dC_c}{dt} = m_o * 9.3 * 10^{-12} * \frac{m_t^{2.5}}{m_o}$$

```
RATES
CCalcite
     if (m <= 0.0) then goto 210
     sr CC = sr("CCalcite")
     if (sr CC >= 1.0) then goto 210
     moles = m0*(7.5e-4/3.15e7) * (m/m0)^3.0 * time * (1-sr CC)
     if moles > m then moles = m
210 save moles
SSiderite
     sr SS = sr("SSiderite")
     moles = (1e-4/3.15e7) * time * (1-sr SS)
210
     save moles
      -end
Fe (OH) 3As
      -start
    if (m <= 0.0) then goto 210
    sr fe = sr("Fe(OH)3As")
     if (sr fe >= 1.0) then goto 210
     moles = m0*(0.8e-3/3.15e7) * (m/m0)^1.5 * time * (1-sr fe)
     if moles > m then moles = m
210
    save moles
      -end
Organic
              -start
      if (m <= 0.0) then goto 20
10
              moles = m0*(2.94e-4/3.15e7) * (m/m0)^2.5
      if moles > m then moles = m
              save moles * time
             -end
```

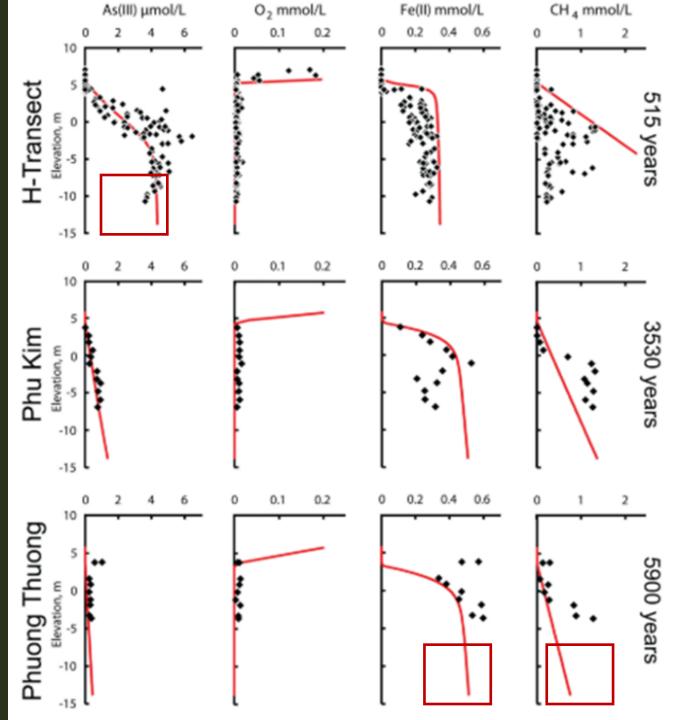
- Kinetics
 - Cell 1
 - Calcite Dissolution
 - Cell 2-40
 - Siderite Precipitation
 - Organic Carbon Degradation
 - Fe-Oxide Reduction
- Transport
 - 6000 Years
 - 20 Meter Vertical Column
- Selected Output

```
KINETICS 1
CCalcite
-m0 10.

KINETICS 2-40
SSiderite
-m0 0.0
Organic
-formula C
-m0 1.36 # 0.27% org C
Fe (OH) 3As
-m0 0.394 #65 umol/g
-bad_step_max 4000
-cvode true
```

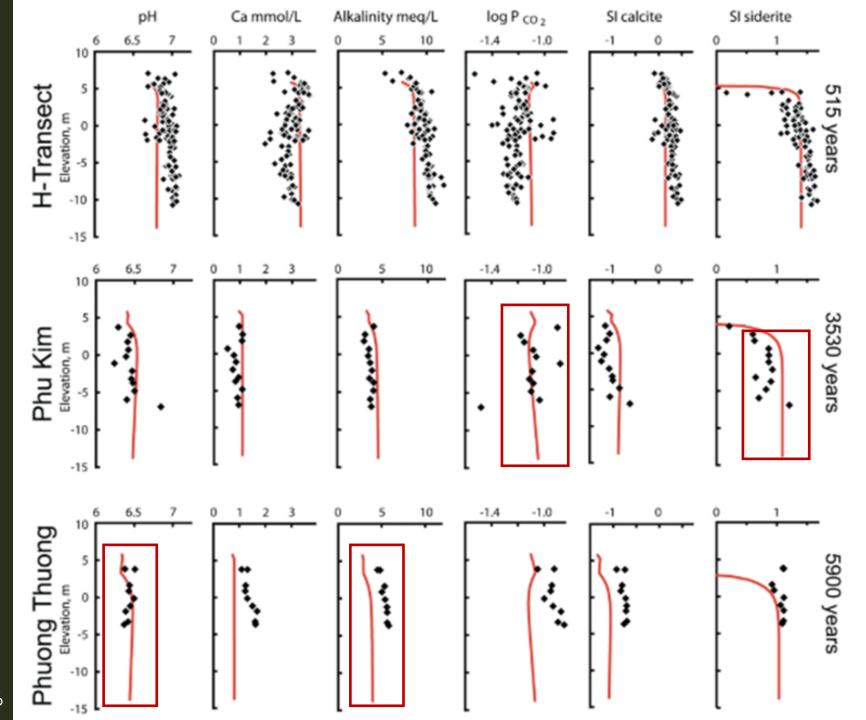
```
TRANSPORT
-cells 40
-shifts 6000
-time_step 31536000 # seconds = 1 year
-lengths 40*0.5
-print_frequency 200
-punch_frequency 200
```

Postma et al. 2016 Results



After 1000 years

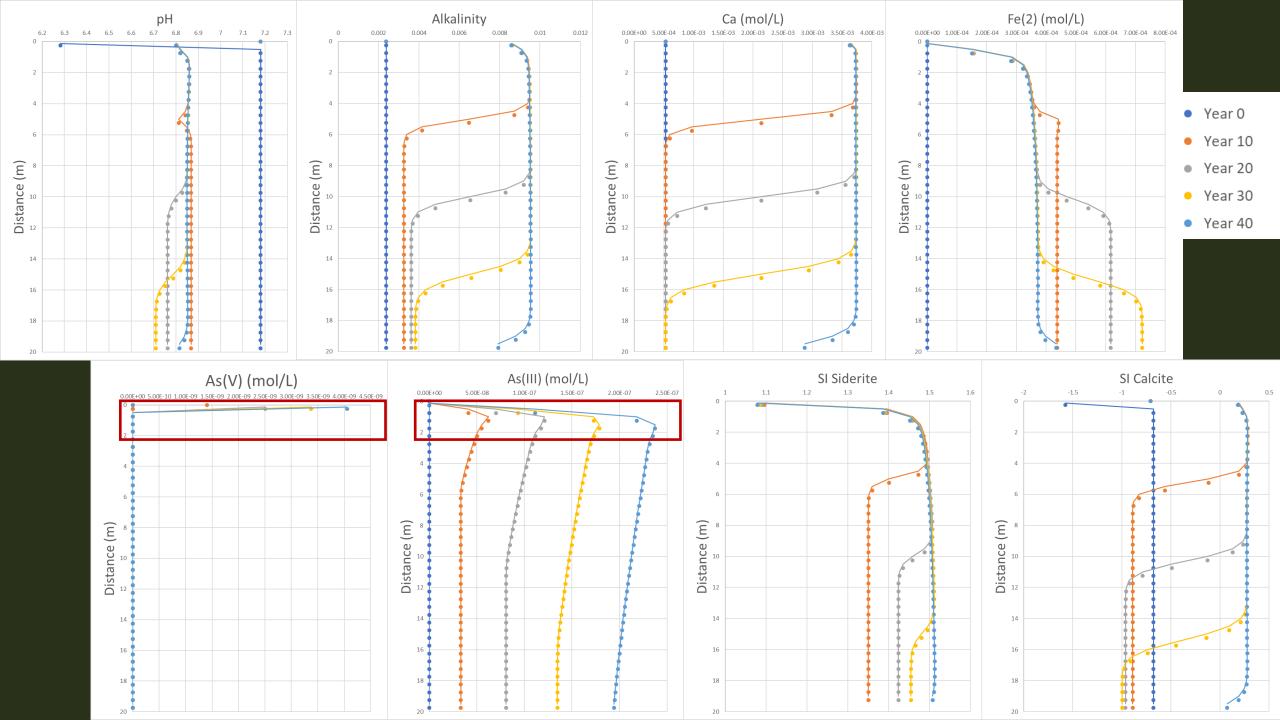
- Reduction in As(III)
- More aqueous Fe(II)
- Less CH₄ Production
- Lower pH
- Lower Alkalinity
- Less stable P_{CO2}
- Siderite Dissolves

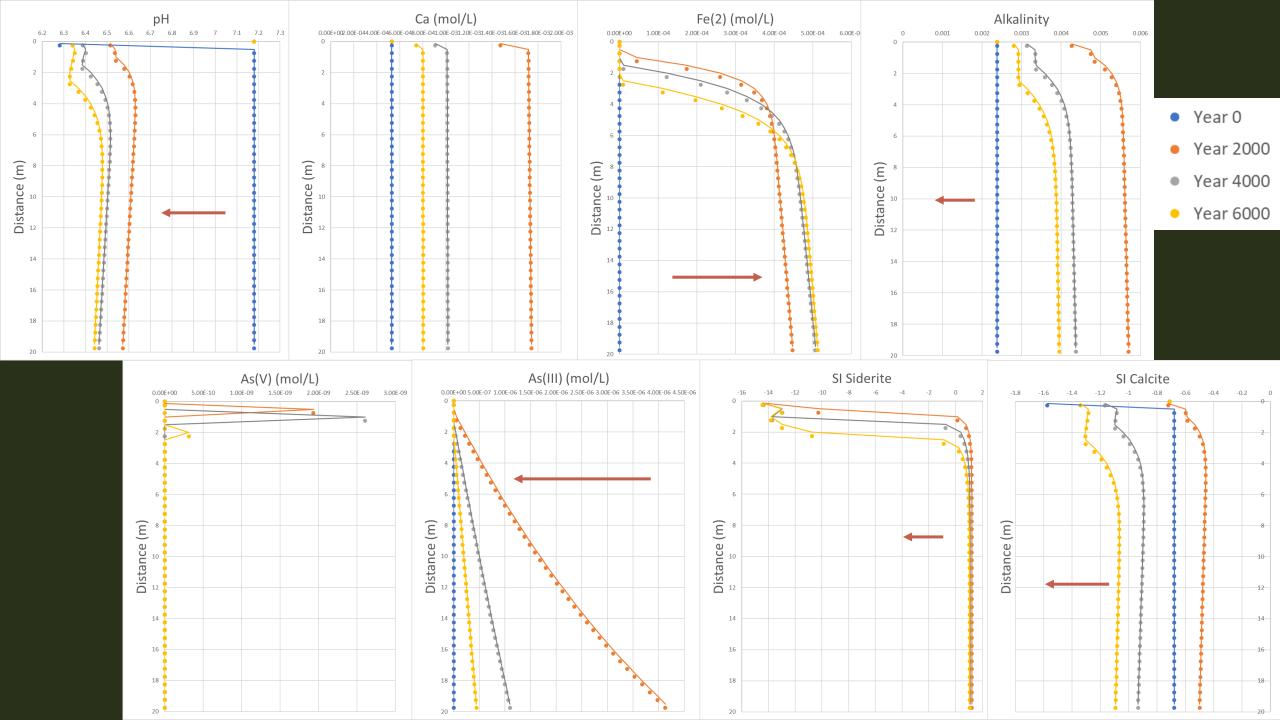


PHREEQC Input Modification

- Transport
 - 40 Cells
 - 0.5 Meters long
 - 20 Meter Vertical Column
 - 40 Shifts
 - 40 years
 - Print Every 5 Shifts

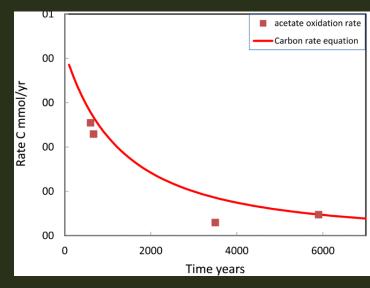
```
TRANSPORT
-cells 40
-shifts 40
-time_step 31536000 # seconds = 1 year
-lengths 40*0.5
-print_frequency 5
-punch_frequency 5
```





Conclusions

- 1. Kinetic reaction rates allow for more accurate longer-term modeling
- 2. Organic carbon reactivity is limiting agent, and is inversely related to time
- 3. Dynamic stability over the first ~1000 years
 - 1. $7CH_2O + 4FeOOH \rightleftharpoons 4FeCO_3 + 3CH_4 + 3H_2O$
- 4. As(III) concentration peaks at ~ 1200 years
 - 1. 600 μg/L 60 times the WHO drinking water limit



Postma et al. 2016

2. At 6000 years concentrations are still more than 3 times the WHO limit

References

- Parkhurst, D. L., & Appelo, C. a. J. (2013). Description of Input and Examples for PHREEQC Version 3 A Computer Program for Speciation, Batch-Reaction, One-Dimensional Transport, and Inverse Geochemical Calculations. U.S. Geological Survey Techniques and Methods, book 6, chapter A43, 497 p. U.S. Geological Survey Techniques and Methods, Book 6, Chapter A43, 6-43A.
- Postma, D., Pham, T. K. T., Sø, H. U., Hoang, V. H., Vi, M. L., Nguyen, T. T., Larsen, F., Pham, H. V., & Jakobsen, R. (2016). A model for the evolution in water chemistry of an arsenic contaminated aquifer over the last 6000 years, Red River floodplain, Vietnam. *Geochimica et Cosmochimica Acta*, 195, 277–292. https://doi.org/10.1016/j.gca.2016.09.014
- Postma, D., Larsen, F., Minh Hue, N. T., Duc, M. T., Viet, P. H., Nhan, P. Q., & Jessen, S. (2007). Arsenic in groundwater of the Red River floodplain, Vietnam: Controlling geochemical processes and reactive transport modeling. *Geochimica et Cosmochimica Acta*, 71(21), 5054–5071. https://doi.org/10.1016/j.gca.2007.08.020
- Thi Hoa Mai, N., Postma, D., Thi Kim Trang, P., Jessen, S., Hung Viet, P., & Larsen, F. (2014). Adsorption and desorption of arsenic to aquifer sediment on the Red River floodplain at Nam Du, Vietnam. *Geochimica et Cosmochimica Acta*, *142*, 587–600. https://doi.org/10.1016/j.gca.2014.07.014